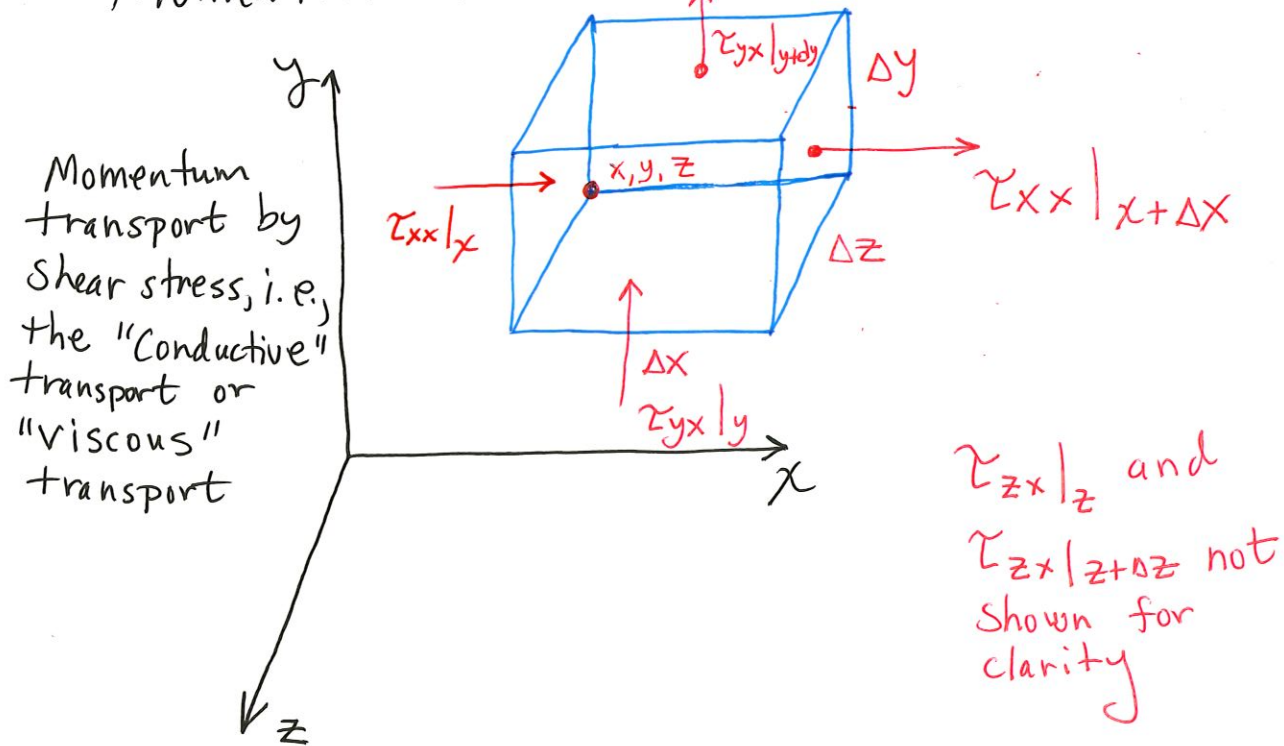


Part 4

Momentum Transfer in x direction



Convective transport is given by:

$$(\rho v_i) v_x = \text{convective flow of x-direction momentum crossing } x, y, \text{ or } z \text{ plane}$$

mass flux crossing x, y, or z plane $i = x, y, \text{ or } z$

Replace τ_{ix} with $v_i v_x$ in above diagram to yield diagram for "convective" part of momentum transport

Viscous transport in terms of momentum/time: (ins-outs parts)

$$\tau_{xx}|_x dz dy - \tau_{xx}|_{x+\Delta x} dz dy + \tau_{yx}|_y dx dz - \tau_{yx}|_{y+\Delta y} dx dz + \tau_{zx}|_z dx dy - \tau_{zx}|_{z+\Delta z} dx dy$$

A similar equation applies for convective transport with $\rho v_i v_x$ replacing τ_{ix}

$i = x, y, \text{ or } z$

Pressure force and gravitational force

$$\Delta y \Delta z (P|_x - P|_{x+\Delta x}) + \rho g_x \Delta x \Delta y \Delta z$$

Accumulation: $(\partial \rho v_x / \partial t) \Delta x \Delta y \Delta z$

Equate and divide by $\Delta x \Delta y \Delta z$ so every term is on a per unit volume basis:

$$\frac{\partial \rho v_x}{\partial t} = - \left(\frac{\partial}{\partial x} \tau_{xx} + \frac{\partial}{\partial y} \tau_{yx} + \frac{\partial}{\partial z} \tau_{zx} \right) - \frac{\partial}{\partial x} \rho v_x v_x + \frac{\partial}{\partial y} \rho v_y v_x + \frac{\partial}{\partial z} \rho v_z v_x - \frac{\partial P}{\partial x} + \rho g_x$$

Accumulation
ins-out + ΣF

More generally, for all three directions, we can write

$$\frac{\partial \rho \vec{v}}{\partial t} = - \underbrace{(\vec{\nabla} \cdot \rho \vec{v} \vec{v})}_{\text{Convective momentum inflow-outflow per unit volume}} - \underbrace{\vec{\nabla} \cdot \bar{\tau}}_{\text{inflow-outflow of momentum by viscous transfer}} - \underbrace{\vec{\nabla} P}_{\text{Pressure force per unit volume}} + \underbrace{\rho \vec{g}}_{\text{gravitational force per unit volume}}$$

Rate of momentum increase per unit volume

Note: $\bar{\tau} = \begin{bmatrix} \tau_{xx} & \tau_{xy} & \tau_{xz} \\ \tau_{yx} & \tau_{yy} & \tau_{yz} \\ \tau_{zx} & \tau_{zy} & \tau_{zz} \end{bmatrix}$ $\tau_{\text{row, column}}$

$$\vec{v} = [v_x, v_y, v_z]$$

$$\vec{v} \vec{v} = \begin{bmatrix} v_x v_x & v_x v_y & v_x v_z \\ v_y v_x & v_y v_y & v_y v_z \\ v_z v_x & v_z v_y & v_z v_z \end{bmatrix}$$

dyadic product
Product is a row vector

Premultiply a matrix by a row vector:

$$[\text{---}] \cdot \begin{bmatrix} | & | & | \\ | & | & | \\ | & | & | \end{bmatrix} = [\text{---}]$$

Use continuity equation to get:

$$\rho \frac{D\vec{v}}{Dt} = -\vec{\nabla}P - \vec{\nabla} \cdot \bar{\tau} + \rho \vec{g}$$

↑ Mass per unit volume times acceleration
↑ Pressure force
↑ Viscous force
↑ gravity force
↖ Equivalent to $F=ma$

General relation between τ_{ij} and velocity gradient:

$$\tau_{yx} = \tau_{xy} = -\mu \left(\frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} \right)$$

$\bar{\tau}$ is symmetric

For ρ and μ constant, and using $\vec{\nabla} \cdot \vec{v} = 0$, the Navier-Stokes equation results:

$$\rho \frac{D\vec{v}}{Dt} = -\vec{\nabla}P + \mu \nabla^2 \vec{v} + \rho \vec{g}$$

For $\vec{\nabla} \cdot \bar{\tau} = 0$, Euler's equation results

$$\rho \frac{D\vec{v}}{Dt} = -\vec{\nabla}P + \rho \vec{g}$$

Forming the "dot" product of the Navier-Stokes equation and \vec{v} yields the microscopic mechanical energy balance (see next page).

Microscopic mechanical energy balance

$$\frac{\partial}{\partial t} \frac{1}{2} \rho |\vec{v}|^2 = -\vec{\nabla} \cdot \frac{1}{2} \rho |\vec{v}|^2 \vec{v}$$

- efflux of kinetic energy
per unit volume

$$-\vec{\nabla} \cdot P \vec{v} - P(-\vec{\nabla} \cdot \vec{v})$$

rate of
work done
by pressure

Reversible
conversion to
internal
energy

$$-(\vec{\nabla} \cdot [\bar{\tau} \cdot \vec{v}])$$

rate of work done
by shear stress

$$-(-\bar{\tau} : \vec{\nabla} \vec{v})$$

Irreversible conversion
to internal energy

$$+ \rho (\vec{v} \cdot \vec{g})$$

Rate of work
done by gravity